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Removing deep brain stimulation artifacts from the electroencephalogram: Issues, recommendations and an open-source toolbox

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Removing deep brain stimulation artifacts from the electroencephalogram: Issues, recommendations and an open-source toolbox



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HIGHLIGHTS

- Antialiasing analog filters are not designed to protect against DBS artifacts in EEG.
- Low-pass temporal filtering is insufficient: DBS also causes low-frequency artifacts.
- Tracking outliers in the frequency domain is necessary to remove DBS artifacts.

ABSTRACT

A major question for deep brain stimulation (DBS) research is understanding how DBS of one target area modulates activity in different parts of the brain. EEG gives privileged access to brain dynamics, but its use with implanted patients is limited since DBS adds significant high-amplitude electrical artifacts that can completely obscure neural activity measured using EEG. Here, we systematically review and discuss the methods available for removing DBS artifacts. These include simple techniques such as oversampling, antialiasing analog filtering and digital low-pass filtering, which are necessary but typically not sufficient to fully remove DBS artifacts when each is used in isolation. We also cover more advanced methods, including techniques tracking outliers in the frequency-domain, which can be effective, but are rarely used. The reason for that is twofold: First, it requires advanced skills in signal processing since no user friendly tool for removing DBS artifacts is currently available. Second, it involves fine-tuning to avoid over-aggressive filtering. We highlight an open-source toolbox incorporating most artifact removal methods, allowing users to combine different strategies.

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Contents

| 1. | Introduction | 2171 |
|----|---|------|
| 2. | DBS artifacts: What do they consist of and why are they so difficult to remove? | 2172 |
| | 2.1. The sampling bias during analog to digital conversion (aliasing effects) | 2172 |
| | 2.2. The filtering bias after data acquisition | 2173 |
| 3. | Systematic review | 2173 |
| 4. | A/D solutions | 2176 |
| | | |

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| | 4.1. | Over-sampling | 2176 | | | | | |
|----|---|---|------|--|--|--|--|--|
| | 4.2. | Analog low-pass antialiasing filters | 2176 | | | | | |
| 5. | Digital solutions | | | | | | | |
| | 5.1. | Low-pass filtering | 2177 | | | | | |
| | 5.2. | Frequency-domain filtering | 2178 | | | | | |
| 6. | Other | Other solutions. | | | | | | |
| | 6.1. | The case of bipolar stimulation | 2179 | | | | | |
| | 6.2. | Searching for short latency (direct) activation of cortex by DBS | 2179 | | | | | |
| | 6.3. | Methods based on DBS pulse detection in the temporal space (template subtraction) | 2179 | | | | | |
| | 6.4. | Independent component analysis (ICA) | 2180 | | | | | |
| 7. | DBSFILT: An open-source matlab toolbox for optimizing artifacts filtering | | | | | | | |
| | 7.1. | Example of combination | 2182 | | | | | |
| 8. | Concl | Conclusion | | | | | | |
| | Ackno | Acknowledgments | | | | | | |
| | Confl | Conflict of interest | | | | | | |
| | Refer | References | | | | | | |
| | | | | | | | | |

1. Introduction

During the past two decades, deep brain stimulation (DBS) has been recognized as an efficient therapy that alleviates the symptoms of various treatment-resistant movement disorders such as Parkinson's disease (PD), dystonia, and tremor (Lyons, 2011; Vidailhet et al., 2013; Aviles-Olmos et al., 2014; Fasano et al., 2014; Kalia et al., 2013; Larson, 2014). Recent reports suggest that DBS can also be effective for treating psychiatric disorders such as depression, obsessive-compulsive disorder, Tourette's syndrome (Holtzheimer and Mayberg, 2011) as well as dementia-related disorders and Alzheimer's disease (Laxton et al., 2013; Hescham et al., 2013). However, the mechanisms underlying the therapeutic success of DBS remain somewhat mysterious (Dostrovsky and Lozano, 2002; McIntyre et al., 2004; Kringelbach et al., 2007; Bourne et al., 2012). While initially conceived as a "reversible lesion", it is increasingly clear that DBS may produce a more complex neurophysiological response (Vitek, 2008; Agnesi et al., 2013; Chiken and Nambu, 2014), not only within but also outside the local circuits targeted by the stimulation. Indeed, the best sites of implantation of the DBS electrodes correspond to regions where the effects of stimulation may be widespread due to activation of multiple pathways (Hammond et al., 2008; Ponce and Lozano, 2010). This is especially the case of the thalamus and subthalamic nucleus (STN), which are at the core of the cortical-thalamic-basal ganglia-cortical network.

Therefore, it is a major issue to understand how DBS of one target area modulates activity in different parts of the brain (Okun, 2014). First, gaining access to the mechanisms of action of DBS may provide important information regarding clinical practice, in particular how some symptoms are alleviated, and how side effects might occur. Second, DBS and associated pathologies also represent important models for studying the neural bases of numerous psychological functions. So far, functional imaging with positron emission tomography (PET) has provided a unique window for analyzing in vivo the consequences of DBS on whole brain activation patterns (e.g., Ballanger et al., 2009a; Ko et al., 2013). Indeed, although possible (e.g., Jech et al., 2001, 2012; Phillips et al., 2006; Holiga et al., 2015), the use of functional magnetic resonance imaging (fMRI) is limited with implanted patients for safety reasons (Rezai et al., 2004; Carmichael et al., 2007). As a consequence, direct assessment remains challenging because PET does not allow event-related analysis of brain activations (e.g., Ballanger et al., 2009b).

Electrophysiological recordings might thus appear as an ideal solution to track brain dynamics under DBS. While local field potential recordings made from the targeted areas of patients undergoing DBS have added greatly to the understanding of the local effects of stimulation (Rosa et al., 2012; Lempka and McIntyre, 2013; Little et al., 2013; Thompson et al., 2014; de Hemptinne et al., 2015), they cannot inform about whole brain dynamics. Electroencephalography (EEG) does. Advanced EEG signal processing methods now allow efficient source separation and localization (e.g., Huster and Calhoun, 2018; Huster and Raud, 2018; Lio and Boulinguez, 2013, 2018; Makeig et al., 2004; Michel and Murray, 2012; Michel et al., 2004; Michel and He, 2011; Pascual-Marqui, 2009; Tang et al., 2005), which permits using EEG to study the effects of DBS on whole brain activity. However, despite increasing interest (Fig. 1), there are still relatively few studies that have analyzed brain activity with EEG during DBS. There are several possible reasons for not using EEG to analyze and localize DBS-induced brain activity modulations. The first one is that it requires sophisticated data analysis to extract useful spatial information from the EEG (Makeig and Onton, 2009). This first limitation can easily be circumvented. Today, several interactive graphic user interfaces (GUIs) offer a wealth of solutions for performing advanced processing of EEG data (e.g., Delorme and Makeig, 2004; Dalal et al., 2004; Delorme et al., 2011; Tadel et al., 2011; Oostenveld et al., 2011). As such, modeling eventrelated brain dynamics with good spatial and optimal temporal resolutions by means of EEG recordings is within reach of all users. The second reason for not using EEG together with DBS is that DBSinduced electrical noise can completely obscure the neural activity of interest (Fig. 2). This second limitation poses more of a problem,



Fig. 1. Growing interest for using EEG to study the effect of STN-DBS on cortical activity, as evidenced by the increasing number of publications in ISI journals and the increasing impact of these studies (cumulated impact = sum of the individual 2014 Journal Citation Reports[®] impact factors for the corresponding period).



Example of EEG signal with and without DBS of the STN

Fig. 2. Topographical and Cz-FCz time-course representations of the effect of STN-DBS on the variance of the EEG signal for one representative parkinsonian patient. Data were acquired with the Biosemi Active Two Mk2 amplifier (Sampling rate: 2048 Hz; Digitalization: 24bit, 4th order Delta-Sigma modulator, $64 \times$ oversampling; Input range: -262 mV to +262 mV). DBS induced artifacts are broadcasted on all electrodes of the scalp, with a signal/noise ratio higher than 1×10^{-3} (-40 dB; $10 \times \text{Log10}$ ($12^2/1200^2$)), as estimated with an amplifier with a low pass response below ~400 Hz).

and the available methods for filtering DBS artifacts are neither easy to use nor fully effective at removing the artifacts (see Erez et al., 2010 for a generalized framework for stimulus artifact removal in electrophysiological recordings). Here, we provide a critical review of the existing solutions, together with a userfriendly and open-source toolbox for combining and optimizing the use of these different techniques.

2. DBS artifacts: What do they consist of and why are they so difficult to remove?

Clinically effective, high-frequency DBS consists in delivering to the targeted structure a train of narrow pulses (60 μ s to \sim 200 μ s), with an amplitude greater than 1 V, at a frequency greater than \sim 100 Hz. This signal is volume-conducted to the scalp, where it produces large artifacts relative to the scale of neural activity measured using typical electroencephalographic recording devices $(10^{-6}$ Volt, Fig. 2). Intuitively, this may not appear to be a serious problem since DBS is applied at a single frequency, which implies that standard analog or digital filters could remove DBS-induced artifacts. Unfortunately, dealing with DBS-induced artifacts is more complex than simply considering the stimulation frequency (Erez et al., 2010), and these artifacts actually affect the entire frequency spectrum, including many physiologically relevant frequency bands. We propose a brief description of the nature and mechanisms of generation of these artifacts before examining the characteristics and limitations of the available filtering methods.

2.1. The sampling bias during analog to digital conversion (aliasing effects)

Recording a continuous physical quantity with a computer device requires that this quantity is converted into a digital signal by sampling at discrete intervals of time. This step is achieved using an analog to digital (A/D) converter, which samples the signal at a predefined frequency. How high should this frequency be to ensure a faithful representation of the continuous EEG signal? In principle, no information is lost in the sampling process if the sampling rate is at least twice the highest frequency in the signal of interest (Nyquist, 1928; Shannon, 1949). However, when the DBS signal is mixed with the EEG signal, the question also arises as to how high should the acquisition frequency be to ensure a faithful representation of the DBS signal? This is not a trivial question because the original signal of DBS pulses is a spike-train in the time domain, i.e., a square wave containing odd frequency harmonics, not a sinusoidal signal as the EEG signal (Fig. 3A). In theory, an extremely high (infinite) sampling rate is thus required to ensure a faithful recording of the DBS signal. In practice, DBS pulses are regularly missed or badly captured by the A/D converter that is limited in its acquisition frequency and amplitude range (Fig. 3B). The probability that a DBS pulse is missed or distorted during recording depends on several factors including the sampling frequency, the type of A/D converter, the DBS frequency, the DBS pulse width and the phase between the DBS signal and the sampling function, the desynchronization between the internal clocks



Fig. 3. Simulation of time domain (left side) and frequency domain (right side) representations of one typical DBS signal (160 Hz, pulse width 60 μs, upper part). **A-**The DBS signal is a spike-train of square signals in the time domain (upper part). In the frequency domain (after fast Fourier transform), the signal is composed of an infinite number of harmonics (only shown up to 5 kHz). Only a 160 Hz sinusoidal signal is made of a single fundamental frequency at 160 Hz without harmonics (lower part). **B-**When the same DBS signal is sampled at 2048 Hz by an A/D converter (left side), the sampling function regularly misses some spikes in the time domain. This creates artifactual signals in the frequency domain, both below and above the fundamental harmonic (aliasing, right side).

of the stimulation and the recording devices. These measurement errors have their own period, leading to artifactual values outside the range of the actual DBS frequency, the so-called aliasing effect (Fig. 3). Moreover, even if the sampling rate is sufficiently high to measure each of the successive peaks in the signal, the jitter between the clocks of the recording and the stimulation devices is further responsible for a non-negligible part of the aliasing effect. Critically, aliased frequencies can contaminate all frequency bands, including frequencies well below the frequency of stimulation (Allen et al., 2010; Jech et al., 2006; Sun et al., 2014).

2.2. The filtering bias after data acquisition

A common solution for suppressing artifacts during postacquisition data processing consists in removing the whole activity contained within the noisy frequency bands. An efficient filter, however, requires that only the noise component at each interference frequency is removed, and that the actual EEG signal content in this frequency band is preserved. It is essential, especially for growing spectral analyses, because the EEG frequency-specific signals provided by time-frequency examination have the potential to disentangle various processes that are known to operate in specific frequency bands (e.g., Albares et al., 2014; Makeig et al., 2004; Siegel et al., 2012). Yet, it could be argued that suppressing the whole signal in the high gamma range (the DBS range) does not matter if the frequencies of interest are below the cut-off. Of course, that only holds if DBS artifacts apply strictly at or above the actual DBS frequency, which is not the case (e.g., Jech et al., 2006; Santillán-Guzmán et al., 2013). The filtering problem thus remains complex yet classical: Using a filter that discriminates between signal and noise.

Within this context, we propose a systematic review to identify and evaluate the techniques available for filtering DBS artifacts from the EEG.

3. Systematic review

We searched the Web of Science and Pubmed databases using the keywords ("EEG" OR "Electroencephalograph* ") AND ("DBS" OR "Deep Brain Stimulation").¹ All human scalp EEG empirical studies during clinically effective high frequency DBS published before 2018 were considered, including methodological studies providing real human data. The analysis returned thirty seven studies, mostly published during the five last years (~57%). For each study, we assessed: (1) the overall strategy appropriated by the authors for removing DBS-induced artifacts, (2) the characteristics of the EEG device/digitization procedure (e.g., sampling rate, A/D converter's internal antialiasing filter, etc.), and (3) the characteristics of the offline digital filtering procedure (e.g., bandpass filtering, Hampel filtering, etc.). Detailed results are presented in Table 1.

In five studies (13%), the issue of removing DBS artifacts was not mentioned, and no specific filtering was implemented. In nine

¹ And all related terminologies.

 Table 1

 Technical solutions identified in the systematic review of all empirical studies published before January 2016 using EEG recordings during clinically effective high frequency DBS in humans.

| Study | | Overall strategy | EEG device/Analog s | olutions | | Offline filtering/Digital solutions | | | | Other | |
|-------------------|-------|---|--|---------------------------------------|-----------------------------------|---|---|---------------------|----------------------|--|--|
| Authors | year | | Model | Analog anti- aliasing filter | A/D conversion | Band pass digital filtering | Frequency domain filtering | | | | |
| | | | | | conversion | | Notch filtering (man.) | Hampel filtering | Matched filtering | | |
| Casula et al. | 2017, | Unknown | BrainAmp 32MRplus, BrainProducts | Unknown | 5000 Hz | Band pass 0.1–1000 Hz | no | No | No | No | |
| Durschmid et al. | 2017 | Notch filters | unknown | Unknown | 256 Hz | Band pass 1–40 Hz | 20 and 50 Hz + 3 harmonics | No | No | No | |
| Kibleur et al. | 2017 | Notch filters | Acticap, Brain Products | Unknown | 2500 Hz resampled at 250 Hz | Band pass 0.6–40 Hz + low pass 30 Hz | Centered on the main harmonics of the stimulation artifact | No | No | Νο | |
| Kim et al. | 2017 | Unknown | GRASS Technologies Corporation | Unknown | 200 Hz | Unknown | No | No | No | No | |
| Miocinovic et al. | 2017 | Negligeable scalp artifacts (considered as confined to frequencies above 50 Hz) | Biosemi ActiveTwo System | Yes but unknown characteristics | 2048 Hz | High pass at 1 Hz | No | No | No | No | |
| Magrassi et al. | 2016 | Unknown | SystemPLUS, Micromed | Unknown | 2018 Hz | Band pass 1–40 Hz | No | No | No | No | |
| Mideksa et al. | 2016 | Notch filter | Simultaneous MEG/EEG (Elekta Neuromag) | Unknown | 2500 Hz | Unknown | Centered on DBS frequency (125– 135 Hz) | No | No | No | |
| Mückschel et al. | 2016 | ICA + digital low pass filtering | Unknown | Unknown | Unknown | Band pass 0.5–20 Hz | No | No | No | Rejection of artefactual ICs after visual inspection | |
| Scholten et al. | 2016a | Negligeable scalp artifacts (bipolar DBS) | BrainVision, Brainproducts | Unknown | 1000 Hz | Band pass 1–200 Hz | No | No | No | Bipolar DBS | |
| Scholten et al. | 2016b | Unknown | BrainVision, Brainproducts | Unknown | Unknown | Band pass 1–200 Hz | No | No | No | No | |
| Sun and Hinrichs | 2016 | Pulse detection in the temporal space and template subtraction | Walter Graphtek EEG recorder | Unknown | 512 Hz | Band pass 0.5–180 Hz | No | No | No | Offline up-sampling, DBS pulse detection, moving average template subtraction with re-sampling. | |
| Gulberti et al. | 2015a | ICA + digital low pass filtering | BrainAmp, Brainproducts | Unknown | 1000 Hz | Low pass < 100 and 48 Hz for time-frequency and power spectrum, respectively | No | No | No | Rejection of artefactual ICs after visual inspection | |
| Gulberti et al. | 2015b | ICA + digital low pass filtering | BrainAmp, Brainproducts | Unknown | 1000 Hz | low pass < 30 Hz | No | No | No | Rejection of artefactual ICs after visual inspection | |
| Markser et al. | 2015 | negligeable scalp artifacts (bipolar DBS) | Unknown | Unknown | Unknown | Unknown | No | No | No | No | |
| Sun et al. | 2015 | Matched filters + notch filters | Synamp2, Neuroscan | Unknown | 1000 Hz | Low pass < 100 Hz | Yes | No | Yes | No | |
| Weiss et al. | 2015 | Negligeable scalp artifacts (bipolar DBS) | BrainAmp, Brainproducts | Unknown | 1000 Hz | Band pass 0.5–200 Hz | No | No | No | Bipolar DBS | |
| Quraan et al. | 2014 | Digital low pass filtering | NeuroScan SynAmps | Low-Pass at 3.5 kHz | 1000 Hz | Band pass 2–20 Hz | No | No | No | Bipolar DBS | |
| Sun et al. | 2014 | Matched filters | Synamp2, Neuroscan | Unknown | 1000 Hz | band pass 0.3-200 Hz | Yes | No | Yes | No | |
| Figee et al. | 2013 | Digital low pass filtering | Advanced Neuro Technology | Unknown | 512 Hz | Band pass 0.5–40 Hz | No | No | No | No | |
| Hohlefeld et al. | 2013 | Digital low pass filtering | NeuroScan SynAmps | Low-Pass at 3.5 kHz | 2000 Hz | Low pass < 30 Hz | No | No | No | No | |

Table 1 (continued)

| Study | | Overall strategy | EEG device/Analog solutions | | | Offline filtering/Digital solutions | | | | Other |
|----------------------------|-------|--|--|--|--------------------------------------|---|----------------------------|---------------------|-------------------|----------------|
| Authors | year | | Model | Analog anti- aliasing filter | A/D conversion | Band pass digital filtering | Frequency domain filtering | | | |
| | | | | | | | Notch filtering (man.) | Hampel filtering | Matched filtering | |
| Santillan-Guzman et al. | 2013 | EMD detrending and manual artifacts rejection by TFDF | Unknown | Unknown | 1000 Hz | no | yes | no | no | TFDF |
| Selzler et al. | 2013 | Digital low pass filtering | NeuroScan SynAmps | Low-Pass at 3.5 kHz | 1000 Hz | Band pass 0.5–50 Hz | No | No | No | No |
| Muthuraman et al. | 2012 | Oversampling + spatial filtering | Unknown | Unknown | Unknown | No | No | No | No | Iterative DICS |
| Walker et al. | 2012a | Oversampling + differential ERPs (Bipolar stimulation) | Unknown | Low-Pass at 3 kHz | 10,000 Hz | No | No | No | No | Yes (DBS ERP) |
| Walker et al. | 2012b | Oversampling + differential ERPs (Bipolar stimulation) | Unknown | Low-Pass at 3 kHz | 10,000 Hz | no | no | no | no | Yes (DBS ERP) |
| Weiss et al. | 2012 | digital low pass filtering | NeuroScan SynAmps | Low-Pass at 3.5 kHz | 1000 Hz | FIR 1–100 Hz + notch 50 Hz | No | No | No | No |
| Cavanagh et al. | 2011 | Digital low pass filtering | NeuroScan SynAmps | Low-Pass at 3.5 kHz | 1000 Hz | low pass at 50 Hz | No | No | No | No |
| Swann et al. | 2011 | Digital low pass filtering | Biosemi ActiveTwo System | Low-Pass first order at 3.6 kHz (3 dB) | 2048 Hz - resampled at 512 Hz | low pass at 50 Hz | No | No | No | No |
| Allen et al. | 2010 | Digital filtering + automatic outlier frequencies suppression | NeuroScan SynAmps | Low-Pass at 3.5 kHz | 1000 Hz | low-pass at 100 Hz, 8th order type II Tchebychev filter, attenuation 40 dB in the stop band. | No | Yes | No | No |
| Klostermann et al. | 2010 | Averaging (standard ERP study) | Unknown | Unknown | 2000 Hz | band pass 0.05–500 Hz | No | No | No | No |
| Weiss et al. | 2011 | Negligeable scalp artifacts (bipolar DBS) | BrainAmp, Brainproducts | Unknown | 5000 Hz – resampled at 1000 Hz | band pass 1–100 Hz | No | No | No | Bipolar DBS |
| Moll et al. | 2009 | High resolution time/ frequency transform | AlphaMap, Alpha- Omega | Low-Pass at 10 kHz | 3000 Hz | band pass 1–300 Hz | No | No | No | No |
| Kovacs et al. | 2008 | Averaging (standard ERP study) | Cambridge Electronic Devices Inc. Power 1401 A/ D converter | Low-Pass at 500 Hz | 1000 Hz | band pass 0.3–30 Hz, 4th order Butterworth IIR filter | No | No | No | No |
| Colloca et al. | 2006 | Digital low pass filtering | Unknown | Unknown | 256 Hz | band pass 6.5–55 Hz | No | No | No | No |
| Frysinger et al. | 2006 | Negligeable scalp artifacts (bipolar DBS) | Unknown | Unknown | unknown | unknown | No | No | No | Bipolar DBS |
| Jech et al. | 2006 | Manual detection and suppression of DBS and aliased frequencies in the frequency domain | Brainscope (M&I) | Unknown | 250 Hz/ 1000 Hz | band pass 0.015–75 Hz/300 Hz | Yes | No | No | No |
| Silberstein et al. | 2005 | Negligible scalp artifacts (bipolar DBS) | Biopotential Analyzer Diana | Unknown | 184 Hz | no | No | No | No | Bipolar DBS |
| Priori et al. | 2001 | Averaging (standard ERP study) | Unknown | Unknown | Unknown | Unknown | No | No | No | No |

G. Lio et al./Clinical Neurophysiology 129 (2018) 2170-2185

DBS = Deep Brain Stimulation; EMD = Empirical Mode Decomposition; TFDF = Time Frequency Domain Filter; DICS = Dynamic Imaging of Coherent Sources.

studies (23.7%) the authors considered DBS artifacts negligible (most often for bipolar DBS and standard ERP studies), and no specific filtering was implemented. In eight studies (21%), a single digital low-pass filter was used to analyze cortical activity in a frequency band lower than the stimulation frequency. In these latter two groups of studies, the possibility of aliasing was ignored. Nine studies (23.7%) considered the aliasing effect and used more sophisticated methods tracking outliers in the frequency domain to identify and remove DBS artifacts above and below DBS the frequency (manual detection and rejection using notch filters, Hampel filtering, matched filters). Three studies (7.9%) combined digital low-pass filtering with independent component analysis (ICA) to identify DBS artifacts as independent components of the EEG signal. Finally, three studies (7.9%) used strategies relying on data acquisition oversampling to allow a more specific analysis of the cortical activity evoked by the stimulation pulse (Muthuraman et al., 2012; Walker et al., 2012a, 2012b). In these studies, specific methods were used to dissociate the cortical signal from the artifactual signal in space (Muthuraman et al., 2012) or in time (Walker et al., 2012a, 2012b).

4. A/D solutions

4.1. Over-sampling

Oversampling is a theoretically sound strategy to reduce aliasing (Fig. 4), but it is practically limited. EEG sampling rate is limited by several factors, especially the number of channels that have to be acquired simultaneously. For instance, the popular Biosemi Active 2 system is limited to a sampling rate of 2048 Hz at the output for 256 electrodes, 4096 Hz for 128 electrodes, 8192 Hz for 64 electrodes, etc. Indeed, the studies identified above that use a sampling rate of 10,000 Hz recorded from no more than 16 electrodes, which poses a serious problem for EEG studies where high density EEG (64–256 channels) is required to perform accurate separation and localization of electrical sources (e.g., Michel et al., 2004).

Oversampling is unquestionably beneficial for any step of the A/ D conversion as well as post-acquisition processing, and the maximum sampling rate should be systematically used before any attempt to filter high frequency DBS artifacts. However, aliasing effects do not vanish at affordable sampling frequencies (Fig. 4), meaning that high sampling is necessary but not sufficient. Future high-resolution EEG systems with sampling frequencies above 10 kHz/128 channels, along with data processing facilities, will be an important advance for the field.

4.2. Analog low-pass antialiasing filters

Almost all recording devices with an A/D conversion step use analog lowpass filters to reduce aliasing effects. These filters are designed to suppress all frequencies above the half of the sampling frequency (the so-called Nyquist-Shannon frequency). The goal is to limit saturation of the analog modulator of the A/D converter and to avoid frequencies above the half of the sampling rate being aliased into the bandwidth of interest. In practice, such filters can distort the signal of interest, are limited in their complexity (filter order), are better suited to filter very high frequencies (~5 kHz) and should not interfere with the oversampling capacity of modern



Fig. 4. Simulation of the aliasing effect for different sampling rates. The same typical DBS signal is used (160 Hz, pulse width 60 µs, upper part). The simulation includes the effect of the antialiasing analog filter (see Figs. 5 and 6). The lower the sampling rate; the higher the number of spikes missed in the time domain, and the higher the number of aliased frequencies in the frequency domain. Residual distortions are observed even for unconventionally high sampling frequencies.

Effect of antialiasing analog filters on a DBS signal



Fig. 5. Illustration of the effect of an antialiasing Butterworth analog filter on a DBS signal (identical parameters as in Fig. 4 are used for this simulation). **A-** The effect on the amplitude of the signal is limited, but the signal is delayed and distorted (the effect increases as the order of the filter increases). This illustration also introduces another problem related to the bias generated by such analog filters for the analysis of DBS-induced event-related potentials (e.g. Baker et al. 2002; MacKinnon et al. 2005; Walker et al. 2012a, 2012b). **B-** Antialiasing analog filters do not completely solve the problem because the DBS transformed signal is still a complex mixing of harmonic components below the cut-off frequency.

A/D converters. Accordingly, these filters are often single pole low pass filters with a cutoff frequency of 3 dB around 3 kHz (Table 1, Fig. 5), far above the fundamental frequency of DBS. Therefore, these filters have a very limited effect on DBS-induced artifacts (Figs. 5, 6).² Fig. 7 shows real data illustrating the fact that artifacts in low frequency bands remain after antialiasing solutions such as analog low-pass filters and oversampling/delta-sigma modulation for A/D conversion. Indeed, these methods are not designed to remove artifacts with a magnitude comparable to that induced by DBS (estimated signal/noise ratio>>–30 dB, Fig. 2).

5. Digital solutions

5.1. Low-pass filtering

Digital filters can be applied online during data acquisition, and/ or offline after the whole signal has been recorded. Digital filters are typically used in data acquisition systems to remove the noise injected during the A/D conversion. Such filters have a cutoff frequency far above the frequency band of interest to limit phase distortions at lower frequencies. Accordingly, offline zero-phase lowpass filters with a cutoff frequency below the stimulation fre-

DBS signal (1V, 160Hz, 60µs) passed through the signal acquisition/pre-processing pipeline

(A) Analog low pass filtering (1st order, 3kHz @ 3dB)







(C) Digital low pass filtering (50 Hz, -80 dB)



(D) FFT (remaining aliased components)



Fig. 6. Illustration of a 1 V, 160 Hz, 60 μ s DBS signal passed through the whole signal acquisition/pre-processing pipeline. **A**- Analog antialiasing filter (Butterworth, First order, Low pass at 3 kHz, 3 dB). The signal amplitude is slightly attenuated, but remains equivalent to a spike train at the stimulation frequency (see Fig. 5). **B**- A/D conversion (sampling rate 1024 Hz). The sampling frequency is too low to adequately capture the DBS signal (aliasing effect, see Figs. 3 and 4). **C**-Offline digital filtering (Two pass, zero-phase, Low pass Chebyshev type II at 50 Hz, Attenuation 80 dB in the stop band.). High frequency components are effectively removed, but a smoothed periodic signal, with an amplitude of more than 2 mV remains. **D**- High resolution amplitude spectrum of the remaining signal. The artifact is composed of harmonics of the stimulation frequency, aliased in the frequency band of interest. Such signal can bias spectral and coherence analyses in low frequency bands and must be removed.

quency are necessary to remove most of the artifacts induced by high frequency DBS. Digital filters have better properties than analog filters, with a sharper roll off and a good attenuation in the stop band. All frequencies above the stimulation frequency are removed with this procedure, but aliased frequencies below the cut-off will remain unchanged. In the temporal domain, the resulting signal is a smoothed periodic signal (Fig. 6) mixed with the actual neurological signal.

Many of the studies we examined applied low-pass filters alone to remove DBS artifacts (e.g., Cavanagh et al., 2011; Figee et al., 2013, etc., Table 1), assuming that DBS-induced high-frequency signals will simply be suppressed from the mixed set of signals recorded at electrodes sites. This is justified if the sampling rate is sufficiently high to avoid any aliasing phenomenon, but in practice the sampling rate is always too low and the magnitude of the DBS-induced electrical noise is too high to neglect aliased frequencies (Jech et al., 2006; Allen et al., 2010). Digital low-pass filtering does not compensate for analog filtering limitations, which was clearly demonstrated by Santillán-Guzmán et al. (2013) who showed that the power spectrum of the low-pass filtered signal in the ON state remains contaminated by comparison to the OFF state control condition. Even with high-performance equipment,

² More information about the physical properties of the analog filter can be found in datasheets issued from the semi-conductor industry (e.g. Baker 1999, Antialiasing, Analog filters for Data acquisition systems, AN699 Microchip Technology Inc).



Using frequency domain filtering in combination with analog and digital low-pass filtering

Fig. 7. Illustration in the frequency domain of the respective effects of the different existing methods for filtering DBS artifacts (Real data). Data were recorded at 2048 Hz from one Parkinsonian patient (152 seconds resting state, eyes closed), with STN DBS delivered at 130 Hz (Left, 3.2 V, 60 μs; Right, 3.0 V, 90 μs), with an EEG device using an analog low pass filter and an oversampling strategy to limit the aliasing effect (BiosemiActiveTwo Mk2 amplifier, Sampling rate: 2048 Hz; Digitalization: 24bit, 4th order Delta-Sigma modulator 64× oversampling; Input range: –262 mV to +262 mV; Low-pass antialiasing analog filter - first order – cutting frequency at 3.6 kHz (3 dB)). **A**- High resolution power spectrum averaged for all electrodes. The fundamental of the stimulation frequency and the two first harmonics are observed at 130, 260 and 390 Hz. Despite the antialiasing features of the high-resolution recording device, aliased frequencies remain. **B**- Same data after low pass filtering (Chebyshev Type II IIR filter, attenuation 120 dB, two-pass zero-phase). Most of the DBS induced artifacts are removed, but aliased frequencies remain in the main frequency bands of interest for EEG analyses. **C**- Automatic detection of outliers in the high resolution power spectrum by the Hampel identifier (dark red line; windows length: 1 Hz; threshold: 2). All frequencies above the Hampel identifier are deemed as artifacts, whenever they are actual aliased frequencies or not. **D**- Same data after identification of aliased spikes. Only spikes above the Hampel identifier are no longer erroneously considered as artifacts in this example. Obviously, the same applies to the 50 Hz powerline, which must be filtered separately. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

simple low-pass temporal filtering is not satisfactory to remove DBS-induced artifacts (Fig. 7).

5.2. Frequency-domain filtering

DBS-induced electrical signal can be assumed as being stationary, i.e., the power spectrum and the phase of the signal that has to be removed are not supposed to change over time. If this assumption is correct, suppressing the remaining low-frequency artifacts after low-pass filtering can be performed by means of frequencydomain filtering techniques since aliased artifacts appear as distinct peaks throughout the frequency spectrum. There are several solutions, but relatively few studies have used this kind of technique (only six were identified in our systematic review, Table 1). It can be implemented by manual detection of the aliased frequencies in the high resolution power spectrum of the data, and application of a set of specifically designed band-stop filters (Jech et al., 2006). A variant of this method based on a hybrid (time/frequency) filtering strategy has later been proposed by Santillán-Guzmán et al. (2013), which is useful when a clear and narrow peak at the stimulation frequency cannot be easily detected in the high resolution power spectrum (i.e. when the stationary assumption has been violated).

However, this kind of technique needs time-consuming and expert analysis of the data, and relatively complex signal processing procedures to preserve the neurological signal around the aliased frequencies. Allen et al. (2010) propose an automatic method to circumvent this problem. After the time-domain signal has been transformed into the frequency domain with the fast Fourier transform (FFT), a Hampel filter is used to identify artifactual frequency peaks, and these peaks are replaced with interpolated values. The Hampel filter is a robust statistic that detects outliers in a sequence as those data points for which the difference from a locally estimated median is greater than a pre-determined threshold (Fig. 7). The cleaned spectrum is then transformed back to the time domain via the inverse FFT. This original method represents a major advance, not only because it can detect aliased frequencies, but also because it has the potential to remove only the noise component at each interference frequency, i.e., to preserve the actual EEG signal in this frequency band. However, for two main reasons, it is less popular than low-pass filtering methods. First, it requires advanced skills in signal processing since there is no user friendly tool for applying these filters. Second, it requires tuning to avoid over-aggressive filtering and a correct detection of the aliased frequencies (Fig. 7C).

Finally, a more recent technique derived from the understanding of the DBS artifact waveform has been proposed by Sun et al. (2014). Provided that the artifacts frequencies can be predicted and are uncorrelated with the underlying signal, matched filters can be applied to remove the unwanted components (Sun et al., 2014). Matched filters offer a valuable alternative to more standard Finite Impulse Response (FIR) and Infinite Impulse Response (IIR) notch filters. Indeed, while notch filters are just centered at the frequency of the sinusoid, matched filters use both the amplitude and phase information of the sinusoidal component for estimation and removal (Kay, 1993). Theoretically, they are better suited for removing DBS-induced artifacts from the EEG signal than other filters, which are less appropriate because of (i) their inability to estimate automatically the strength of the unwanted component (the attenuation of classical FIR and IIR notch filters has to be determined by the experimenter) and (ii) their spectral spread which leads to suppression of surrounding frequencies as well (Sun et al., 2014). Matched filters can be applied by estimating the phase and the amplitude of an unwanted frequency by calculating the cross-correlation between the noisy EEG signal and an artifact component template (ibid).

Obviously, the critical point with frequency-domain filtering techniques is the accuracy with which artifactual frequencies can be identified. Indeed, aliased frequencies are not a simple function of DBS frequency and acquisition rate, but rather comprise a range of frequencies around the expected component frequency (e.g., Sun et al., 2014). The reason is that the Shannon-Nyquist theory used to predict the frequencies of both the natural and aliased harmonics assumes an ideal A/D conversion while in practice EEG devices have non-linear A/D-Converters like Delta-Sigma modulators. Another reason is clock jittering (Sun and Hinrichs, 2016). The internal clock of the stimulation and the recording devices do not have identical resolution, and are not perfectly synchronized. In consequence, even if the sampling rate is high, all stimulation pulses are not measured exactly in the same manner. This leads to low frequency variations within stimulation pulse recordings, and creates artificial low-frequency components at frequencies below the stimulation frequency. In other words, several phenomena may occur in commercial A/D-Converter that can make aliased frequencies difficult to predict, like periodic saturations of the quantizer, periodic quantization noise, clock jitter, etc. (see Pamarti, 2010; Gaggl, 2013; Sun and Hinrichs, 2016). Unfortunately, many of these parameters are often unknown to the user. The relative unpredictability of aliased frequencies has been highlighted in previous papers (e.g., Jech et al., 2006) and is further illustrated in the present review (Fig. 4). Yet, in any case, it is highly recommended to use high resolution measurement techniques to identify aliased frequencies more accurately before removing them with any frequency-domain filtering technique.

6. Other solutions

6.1. The case of bipolar stimulation

It has been suggested that bipolar DBS stimulation produces clinically insignificant artifacts (Frysinger et al, 2006; Silberstein et al., 2005; Quraan et al., 2014). In a (pseudo)-monopolar configuration, the pulse generator serves as the anode and an intracranial contact as the cathode. This configuration generates a long-dipole electrical field. In a bipolar configuration, intracranial electrodes serve both as the anode and the cathode. This configuration generates a short electrical dipole, and thus involves a smaller volume of tissue. Accordingly, it is sometimes believed to generate negligible artifacts (Frysinger et al., 2006). However, as demonstrated in several studies (Baker et al, 2002, MacKinnon et al., 2005; Walker et al. 2012a,2012b), bipolar DBS stimulation does actually produce significant artifacts (Fig. 8). In addition, the scope of this method is limited because most DBS patients undergo monopolar stimulation. Indeed, usually, at the initial programming of DBS parameters, monopolar stimulation is employed. The patient is switched to bipolar stimulation only if an optimal setting (combining pulse width, frequency, voltage, and electrode configuration) is not reached (Wagle Shukla and Okun, 2014).

6.2. Searching for short latency (direct) activation of cortex by DBS

Studies interested in how DBS synchronizes cortical activity to the stimulation frequency are a special case, and need specific solutions for filtering DBS artifacts. One consists in implementing analytical techniques that reverse the anode and cathode electrode contacts and sum the resulting pair of potentials evoked by bipolar DBS (Walker et al. 2012a,2012b). This technique requires an extremely high sampling rate during data acquisition.

Another approach is based on the use of head models coupled with beamforming techniques to identify the network which oscillates at the same frequency than the DBS (Muthuraman et al., 2012). The method assumes that the spatial signature of the DBS signal is identifiable with satisfactory resolution, i.e., can be isolated from other sources by means of spatial filters.

6.3. Methods based on DBS pulse detection in the temporal space (template subtraction)

Provided that the amplitude of the stimulation artifact is substantial and the acquisition frequency is sufficiently high, thresholding in the temporal domain can be used to better identify stimulation artifacts. This technique is similar to the template subtraction techniques used to reduce gradient artifacts during EEGfMRI recordings (e.g. Becker et al., 2005). Sun and Hinrichs (2016) recently proposed a resampling strategy that consists in removing DBS artifacts by subtracting adaptive DBS artifact templates from the contaminated data (Fig. 9). Importantly, the major advantage of this method is that it allows precise reconstruction of the artifact shape without the need to oversample the signal during A/D conversion. According to Sun and Hinrichs (2016), this technique is especially beneficial for analyzing activity in higher frequency bands (gamma activity). However, the method does have potential drawbacks. DBS artifact subtraction requires stimulation based epoching (data alignment on the basis of peak detection). Yet, due to the desynchronization of the internal clocks of the recording and stimulation devices, the technique induces a substantial increase of the number and amplitude of aliased frequencies in lower frequency bands (Fig. 9). In addition, DBS artifact subtraction has a considerable potential to introduce strong biases in the spectral signal, as illustrated in Fig. 9. This was not evidenced in Sun and Hinrichs' original investigation probably because their dataset was weakly contaminated by DBS artifacts (no more than a factor 10). It is much more common for DBS artifacts to reach a factor of 1000 (see Fig. 2). As a consequence, given that the noise introduced in the frequency spectrum by stimulation based epoching increases as a function of artifacts amplitude (Fig. 9), it is likely that the method is less efficient with more noisy datasets. In conclusion the method might be convenient for studies focusing on direct (short-latency) activation of the cortex by the stimulation pulse, or bipolar stimulation, but some caution is advised when data processing is concerned with analyses in the spectral domain.



Effect of bipolar STN stimulation

Fig. 8. Four-second excerpts of waking EEG from one subject with bilateral subthalamic nuclear (STN) deep brain stimulation (DBS) for Parkinson disease. (A) Bilateral DBS on in bipolar mode. (B) Both DBS implants off. (3.0 V, case +, 0–, 160 Hz, 90 microseconds. Bar = 100 µV; time marks = 1 second). Reproduced with permission from: Frysinger et al. Neurology 2006; 66:268–270. ©2006 by Lippincott Williams & Wilkins.

6.4. Independent component analysis (ICA)

The general strategy assuming that the signature of the DBS signal can be isolated from the other electrical sources with which it is mixed to form scalp potentials DBS (see above Muthuraman et al., 2012) opens up new perspectives regarding the use of spatiotemporal techniques like ICA to optimize DBS artifacts filtering. Three recent studies (Gulberti et al., 2015a, 2015b; Mückschel et al.,2015) paved the way for this solution. ICA is the most popular blind source separation (BSS) method, a data-driven technique that allows the separation of signals from a set of mixed signals contributing to the overall electrical activity recorded on the scalp. Importantly for the present issue, it is performed with no need of information about the sources or the mixing process. As applied to EEG data, ICA most often uses higher order statistics (HOS) to decompose the raw signal obtained from a specific number of electrodes into the same number of statistically maximally independent components (Delorme et al., 2007; Onton and Makeig, 2006). It has long been employed by EEG users to reject artifacts like eye blinks, saccades, cardiac activity and most of the Gaussian noise. Given the efficiency of the method for denoising classical EEG recordings, the method seems applicable in this instance. However, regarding the unfavorable signal/noise ratio between the DBS artifact and the neuronal sources (Fig. 9), more work has to be done to find a solution that preserves the physiological signal when focusing on whole brain dynamics. One particular difficulty with this method is highlighted in Fig. 10, which shows that whatever the properties of the algorithm used for source separation (Lio and Boulinguez, 2013), DBS spikes can still be found in most sources. This demonstrates that the signature of the DBS signal is not easily identifiable as a single -or a set of- independent component-s-.

7. DBSFILT: An open-source matlab toolbox for optimizing artifacts filtering

Studies on the global effect of DBS (i.e., the effect on the whole EEG spectrum which is supposed to mediate the variety of cognitive and sensorimotor processes modulated by stimulation) require rigorous DBS filtering. The considerations above indicate that no single approach can efficiently remove DBS artifacts from the EEG. Rather, we argue that the techniques of data acquisition and data processing examined can be effectively combined. For this purpose, we have developed an open-source toolbox (DBSFILT) that integrates some of the useful methods for filtering DBS artifacts, as well as routines for optimizing their efficacy. DBSFILT is free software, and we aim to continually including new solutions, scripts, databases, commentaries, or any other contributions to promote collaborative development dedicated to providing optimal solutions to removing DBS artifacts. We have conceived DBSFILT as a starting point for contributors to share their techniques and code in order to allow users to choose the most efficient combination of methods according to the specific conditions under which their signal has been acquired.

Some of the useful functions to date for DBS filtering (low-pass filtering, Hampel filtering with aliased spikes identification, matched filters, automatic detection of the DBS pulses in the temporal domain, etc.) are included in DBSFILT with examples (including data from Fig. 7), tutorials, and a graphical user interface for

Template subtraction

(DBS: 130Hz synchronized left and right subthalamic nuclei; Sampled at 2048 Hz with a Delta-Sigma A/D converter; upsampled to 20480 Hz)

(A) High-pass filtering + Upsampling + Peak detection by thresholding in the temporal domain + Detection-based epoching + Spectral analysis



(B) Signal reconstruction after suppression of aliased frequencies



Fig. 9. Moving average template subtraction. (A) High resolution power spectra displayed for raw and aligned signal (re-epoching is based on stimulation peaks detection). The method allows a better definition of the artifact in the high resolution power spectrum around the stimulation frequency. This can be highly beneficial when the stimulation frequency is low and overlaps the frequency band of interest. However, the method can induce substantial increase in the number and amplitude of aliased frequencies in lower frequency bands, as illustrated in the power spectrum of stimulation-based epoched data. Relative power spectral density shows large increases in power due to data alignment, either in the form of increased burst (e.g., 33 Hz) or constant drift (e.g., 75 Hz). The % of signal change after data alignment is strongly correlated with the artifact to background amplitude ratio. (B) Signal reconstruction after moving average template subtraction (red) and low-pass + frequency domain filtering (Hampel).

Using ICA to isolate artifacts as independent components (ICs)

(DBS: 130Hz synchronized left and right subthalamic nuclei; Sampled at 2048 Hz with a Delta-Sigma A/D converter; 10 electrodes -> 10 ICs)



Fig. 10. Using ICA to isolate artifacts as independent components. In this illustration, DBS artifact is not identified as an independent component. (A) When low-pass filtering is not applied, DBS signal is not separated from the other sources, and the powerful 130 Hz peak (DBS frequency) is observed within the mean amplitude spectrum of all sources (only 9 are shown for convenience). (B) When low-pass filtering is applied, aliaised frequencies can still be observed within the mean amplitude spectrum of most sources (6/10, only 2 are shown for convenience).

interactive use. Users can test and combine the different solutions available in order to run the method which best fits the specific needs of their dataset.

This toolbox can be downloaded at:

https://github.com/guillaumelio/DBSFILT/releases

A tutorial can be found on the download platform (technical document: DBSFILT/DBSFILT_GUI_DOC.pdf).

7.1. Example of combination

All methods have advantages and caveats, and below we outline a combined approach and illustrate how it is implemented in our toolbox. We recommend using a mixed approach combining complementary solutions: high sampling rate, analog low-pass filtering, digital low-pass filtering, and frequency-domain filtering guided by artifact identification procedures.

In the method proposed by Allen et al. (2010), the efficiency of the Hampel filter depends on parameters controlling the sensitivity of the filter. As put forward by the authors, the filter is blind. It does not require a priori knowledge of which frequencies to process. Threshold values are determined according to the number and the intensity of the aliased frequencies that can be detected in the high-resolution power spectrum. In other words, setting parameters relies mostly on the characteristics of the data acquisition procedure (sampling rate, A/D conversion) and on the length of the recorded data (spectral resolution). This procedure is convenient because identical parameters are suitable for all subjects, regardless of their individual stimulation parameters. However, this method is often too aggressive and tends to consider as outliers frequency peaks that do not correspond to aliased frequencies (Fig. 7C). In order to avoid this potential bias, we have included a method in the DBSFILT toolbox to guide the filter towards the frequencies at which DBS artifacts are likely to occur. These frequencies are a function of the individual stimulation parameters. Aliased frequencies are typically captured in the high-resolution power spectrum as outlier frequencies that are sub-multiples of the stimulation frequency (Jech et al., 2006, Fig. 7a). The algorithm calculates all possible aliased frequencies and allows automatic removal by the Hampel filter only when the outliers correspond to these frequencies (Fig. 7D):

$$f_{spike} = \mathbf{h} \times \left(\frac{f_{DBS}}{n} \right); \text{ where } \mathbf{h} = h \pm \varepsilon; \ h \in \mathbb{N}^+ \text{ and } n < n_{max} \in \mathbb{N}^+$$

where:

 f_{spike} is the outlier frequency detected by the Hampel filter, f_{DBS} the stimulation frequency,

n the number of consecutive DBS pulses missed (or differently captured (Sun and Hinrichs, 2016)) by the ADC + 1,

 n_{max} the estimated maximum number of consecutive DBS pulses missed (or differently captured) by the ADC + 1,

h define the harmonics of the aliased signal,

 ε a small number describing the tolerance for DBS spike identification (dealing with the clock accuracy of the sampling and the stimulation device).

Only the stimulation frequency, n_{max} and the ε parameters have to be set by the user (typical values for the A/D and DBS parameters described in the simulations and real data presented in the present paper: $n_{max} = 10^\circ$; $\varepsilon = 0.001$. $n_{max} = 20^\circ$; $\varepsilon = 0.01$).

8. Conclusion

Advanced signal processing methods now make EEG an ideal tool to track brain dynamics with satisfactory spatial resolution and optimal temporal resolution in healthy subjects. However, in patients, removing DBS artifacts from the EEG is currently not straightforward. Our review of the existing methods indicates that no single approach can efficiently remove DBS artifacts from the EEG. Due to the desynchronization between the stimulation and the recording device, aliased frequencies are introduced in the signal. Oversampling is theoretically sound, but sufficient oversampling is currently impossible for high-density EEG. In addition, it is inadvisable to rely on the analog antialiasing filters of EEG

Recommendations for optimal filtering of DBS-induced artifacts



Fig. 11. Issues and recommendations for removing high frequency deep brain stimulation artifacts from the electroencephalogram.

devices because they are not designed to suppress artifacts of such a magnitude. It is also not appropriate to rely on digital low-pass filtering alone since DBS artifacts are also composed of lowfrequency components. Frequency-domain filtering techniques are efficient, provided that a routine guiding the filter towards the likely artifactual frequencies is used. However, these methods can be used effectively in combination (oversampling, analogic and digital filtering). Issues and recommendations for an efficient use of these techniques are synthetized in Fig. 11. In any case, any spectral difference observed between ON and OFF stimulation conditions still has to be considered with caution. By offering an open-source toolbox which integrates useful functions for DBS filtering, we hope to stimulate new studies aiming to unravel the controversial nature of DBS effects on whole brain dynamics using EEG.

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Conflict of interest

We declare that we have no conflict of interest.

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